

## Modeling the electronic band-structure of strained long-wavelength Type-II superlattices using the scattering matrix method

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**Abstract:** This study introduces a comprehensive theoretical framework for accurately calculating the electronic band-structure of strained long-wavelength InAs/GaSb type-II superlattices. Utilizing an eight-band  $k \cdot p$  Hamiltonian in conjunction with a scattering matrix method, the model effectively incorporates quantum confinement, strain effects, and interface states. This robust and numerically stable approach achieves exceptional agreement with experimental data, offering a reliable tool for analyzing and engineering the band structure of complex multi-layer systems.

**Key words:** Type-II superlattices, Long-wavelength infrared (LWIR), Scattering matrix method, Electronic band-structure modeling, InAs/GaSb heterostructures, Infrared photodetectors, and Bandgap engineering

### Introduction

Type-II InAs/GaSb superlattices (T2SLs), formed by alternating InAs and GaSb layers over multiple peri-

ods, were first proposed by Sai-Halasz, Tsu, and Esaki in 1977<sup>[1]</sup>. These structures are characterized by a broken-gap alignment where the valence band maximum of GaSb lies above the conduction band minimum of InAs,

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She joined Northwestern University, Evanston, IL, as a Walter P. Murphy Professor and Director of the Center for Quantum Devices in Fall 1991, where she created the undergraduate and graduate program in solid-state engineering.

She has authored or co-authored more than 1000 papers, more than 35 book chapters, and 20 books, including the textbooks Technology of Quantum Devices (Springer Science Business Media, Inc., New York, NY U. S. A. 2010) and Fundamentals of Solid State Engineering, 4th Edition (Springer Science Business Media, Inc., New York, NY U. S. A. 2018). Two of her books, MOCVD Challenge Vol. 1 (IOP Publishing Ltd., Bristol, U. K., 1989) and MOCVD Challenge Vol. 2 (IOP Publishing Ltd., Bristol, U. K., 1995), discuss some of her pioneering work in InP-GaInAsP and GaAs-GaInAsP based systems. The MOCVD Challenge, 2nd Edition (Taylor & Francis/CRC Press, 2010) represents the combined updated version of Volumes 1 and 2. She holds many U. S. patents and has given more than 1000 invited and plenary talks. Her current research interest is in nanoscale optoelectronic quantum devices. From deep UV to Thz.

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resulting in the spatial separation of electrons in InAs and holes in GaSb. The tunable band-structure of T2SLs is one of their most significant advantages, as the energy gap can be engineered by varying the layer thicknesses and interface compositions. This tunability makes T2SLs a promising candidate for a wide range of applications, including photodetectors [2, 3] and lasers [4]. In particular, their narrow bandgap makes them especially well-suited for the development of long wavelength infrared (LWIR) photodetectors [3, 5-7].

Traditionally, methods such as the Empirical Tight Binding Method (ETBM) have been used to calculate electronic band structures in these systems [8]. However, ETBM heavily relies on material-specific fitting parameters, limiting its accuracy for narrow bandgaps relevant to LWIR applications. An alternative approach based on the  $k \cdot p$  model and envelope function approximation offers improved accuracy by incorporating interface effects and strain.

In this work, we adopt an eight-band  $k \cdot p$  model to construct the bulk states in individual material layers and match the wavefunctions at interfaces using the boundary conditions from Burt's envelope function theory [9]. This approach accounts for the impact of lattice-mismatch strain on the electronic band-structure of InAs/GaSb superlattices designed for LWIR photodetectors (around the  $\Gamma$ -point). To solve the eigenvalue problem, we employ the scattering-matrix method, which provides greater numerical stability than traditional transfer-matrix approaches, particularly for thicker structures and large basis sets (such as LWIR T2SLs). This method relies on fewer empirical parameters, incorporates strain and interface effects, and reduces computational complexity by handling smaller matrices. At the end, we compare the obtained results from the model with experimental results to confirm the predictions of this method.

## 1 Method

In this work, we consider a structure consisting of InAs/GaSb quantum wells grown along the [001] direction on a GaSb substrate ( $z$ -direction). While the study of bulk materials using the  $k \cdot p$  model does not pose significant challenges, this is not the case for heterostructures like superlattices. The behavior of the envelope function at the interfaces between different semiconductors remains uncertain. However, Burt demonstrated that a Hamiltonian similar to the one proposed by Kane can be effectively applied to the bulk regions of a superlattice, provided the quadratic valence band terms are properly symmetrized [9]. This approach was later extended to an eight-band Hamiltonian by Foreman [10]. This eight-band  $k \cdot p$  model is employed for zinc-blende crystals to describe the conduction and valence band structures near the  $\Gamma$ -point, with spin-orbit coupling and strain effects included. In this model, the contributions of higher bands are neglected, and spin-orbit coupling is treated as a perturbation [11]. Using the following basis functions

$|S \uparrow\rangle, |X \uparrow\rangle, |Y \uparrow\rangle, |Z \uparrow\rangle, |S \downarrow\rangle, |X \downarrow\rangle, |Y \downarrow\rangle,$  and

$|Z \downarrow\rangle$  [10], the  $8 \times 8$   $k \cdot p$  Burt's Hamiltonian can be expressed as:

$$H = \begin{bmatrix} H_4 & 0 \\ 0 & H_4 \end{bmatrix} + H_{so} + H_\epsilon \quad (1)$$

where  $H_4$  represents the  $k$ -dependent  $4 \times 4$  block,  $H_{so}$  accounts for spin-orbit coupling effects, and  $H_\epsilon$  incorporates the strain-induced modifications in the electronic structure.

The  $H_4$  block is defined as:

$$H_4 = \begin{bmatrix} H_{cc} & H_{cv} \\ H_{vc} & H_{vv} \end{bmatrix}. \quad (2)$$

where the conduction band term is  $H_{cc} = E_c(z) + kA_c(z)k$ , with  $A_c$  representing contributions from remote bands [10]. The parameter  $A_c$  is given by:

$$A_c = \frac{\hbar^2}{2m_c} - \frac{P^2}{3E_g} - \frac{P^2}{3(E_g + \Delta)} \quad (3)$$

where  $m_c$  is the conduction band effective mass,  $P$  is the interband momentum matrix element defined as  $P = (\hbar/im) \langle Sp_x | X \rangle$ ,  $E_g$  is the bandgap,  $\Delta$  represents the spin-orbit splitting energy, and  $m$  is the free-electron mass.

The coupling between the conduction and valence bands is expressed as  $H_{cv} = H_{vc}^\dagger = [iPk_x, iPk_y, iPk_z]$ , where Kane's  $B$ -parameter is neglected. The valence band block  $H_{vv}$  is a  $3 \times 3$  matrix that describes the interactions among heavy-hole, light-hole, and split-off states with typical diagonal and off. Its diagonal components are given by:

$$H_{xx} = E_v - \frac{\Delta}{3} + L'K_x^2 + M(k_y^2 + k_z^2), \quad (4)$$

$$H_{xy} = k_x N'_+ k_y + k_y N_- k_x,$$

where  $E_v$  is the valence band edge. Other components are obtained through cyclic permutations of  $x$ ,  $y$ , and  $z$ .

The coefficients  $L'$ ,  $M$ ,  $N'_+$ , and  $N_-$  are derived from the modified Luttinger parameters  $\gamma_1$ ,  $\gamma_2$ , and  $\gamma_3$ . Explicitly, these are defined as

$$L' = -\frac{\hbar^2}{2m}(\gamma_1 + 4\gamma_2), \quad (5)$$

$$M = -\frac{\hbar^2}{2m}(\gamma_1 - 2\gamma_2),$$

$$N'_+ = -\frac{\hbar^2}{2m}(6\gamma_3),$$

$$N_- = M - \frac{\hbar^2}{2m},$$

$$N'_+ = -N'_- - N_-.$$

The modified Luttinger parameters themselves account for remote band interactions and are expressed as

$$\gamma_1 = \gamma_1^L - \frac{E_p}{3E_g}, \quad (6)$$

$$\gamma_2 = \gamma_2^L - \frac{E_p}{6E_g},$$

$$\gamma_3 = \gamma_3^L - \frac{E_p}{3E_g},$$

where

$$E_p = \frac{3m/m_c}{\frac{2}{E_g} + 1/(E_g + \Delta)} \quad (7)$$

and  $\gamma_1^l$ ,  $\gamma_2^l$ , and  $\gamma_3^l$  are original Luttinger parameters. These parameters refine the representation of heavy-hole and light-hole masses and include effects from high-energy bands.

Spin-orbit coupling is represented by  $H_{SO}$ , a matrix term that introduces band splitting due to the interaction between electron spin and crystal field potential. It is given by:

$$H_{SO} = -\frac{\Delta}{3} \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & i & 0 & 0 & 0 & 0 & -1 \\ 0 & -i & 0 & 0 & 0 & 0 & 0 & i \\ 0 & 0 & 0 & 0 & 0 & 1 & -i & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & -i & 0 \\ 0 & 0 & 0 & i & 0 & i & 0 & 0 \\ 0 & 1 & -i & 0 & 0 & 0 & 0 & 0 \end{bmatrix}. \quad (8)$$

Strain-induced effects are incorporated through  $H_\epsilon$ , which modifies the band-structure by accounting for lattice deformation. It can be expressed as<sup>[12]</sup>:

$$H_\epsilon = \begin{bmatrix} H_{\epsilon 0} & 0 \\ 0 & H_{\epsilon 0} \end{bmatrix} \quad (9)$$

where  $H_{\epsilon 0}$  is a  $4 \times 4$  block given by:

$$H_{\epsilon 0} = \begin{bmatrix} a_c \epsilon & 0 & 0 & 0 \\ 0 & h_{xx} & n\epsilon_{xy} & n\epsilon_{xz} \\ 0 & n\epsilon_{yx} & h_{yy} & n\epsilon_{yz} \\ 0 & n\epsilon_{zx} & n\epsilon_{zy} & h_{zz} \end{bmatrix}. \quad (10)$$

In this matrix,  $\epsilon_{ij}$  represents the strain tensor components,  $\epsilon = \epsilon_{xx} + \epsilon_{yy} + \epsilon_{zz}$ , and  $a_c$  is the conduction band deformation potential. The diagonal terms,  $h_{xx}$ ,  $h_{yy}$ , and  $h_{zz}$ , are defined as:

$$h_{xx} = l\epsilon_{xx} + m(\epsilon_{yy} + \epsilon_{zz}), \quad (11)$$

$$h_{yy} = l\epsilon_{yy} + m(\epsilon_{xx} + \epsilon_{zz}),$$

$$h_{zz} = l\epsilon_{zz} + m(\epsilon_{xx} + \epsilon_{yy}),$$

where  $l$ ,  $m$ , and  $n$  are parameters expressed in terms of the valence band deformation potentials  $a_v$ ,  $b$ , and  $d$  as<sup>[12]</sup>:

$$l = a_v + 2b, \quad (12)$$

$$m = a_v - b,$$

$$n = \sqrt{3} d.$$

The strain tensor components are given by<sup>[13]</sup>:

$$\epsilon_{xx} = \epsilon_{yy} = \frac{a_0 - a}{a}, \quad (13)$$

$$\epsilon_{zz} = -\frac{2C_{12}}{C_{11}} \epsilon_{xx},$$

$$\epsilon_{xy} = \epsilon_{yx} = \epsilon_{xz} = \epsilon_{zx} = \epsilon_{yz} = \epsilon_{zy} = 0.$$

Here,  $a_0$  and  $a$  represent the lattice constants of the substrate and the layer material, respectively, while  $C_{11}$  and  $C_{12}$  are the stiffness constants<sup>[14]</sup>.

After composing Hamiltonian matrix, one needs to find eigenvalues. To address the issue of spurious unphysical solutions,  $A_c$  is set to zero<sup>[10]</sup>, simplifying the calculations for the envelope functions  $\psi_i$ . The system is governed by the eigenvalue equation:

$$\sum_{j=1}^9 H_{ij} \psi_j = E \psi_i, \quad i = 1, 2, \dots, 8 \quad (14)$$

where  $E$  is the energy eigenvalue. The scattering matrix method<sup>[15]</sup> is used to solve this equation. This method is particularly effective for determining the subband dispersions and wave functions in multilayer structures with thick layers. Unlike the transfer-matrix method, which is prone to numerical instability due to the equal treatment of exponentially growing and decaying wave functions, the scattering matrix allows the physically significant eigenstates to dominate. This prevents the loss of decaying wave functions during computation and avoids the need for truncation schemes, making it especially effective for accurately analyzing complex band structures in multilayer systems.

The conduction band envelope functions  $\psi_1$  and  $\psi_5$  are expressed in terms of valence band envelope functions as:

$$\psi_1 = i(E - E_c - a_c \epsilon)^{-1} P(k_x \psi_2 + k_y \psi_3 + k_z \psi_4), \quad (15)$$

$$\psi_5 = i(E - E_c - a_c \epsilon)^{-1} P(k_x \psi_6 + k_y \psi_7 + k_z \psi_8).$$

Substituting these expressions into the remaining six equations reduces the system to a  $6 \times 6$  energy-dependent Hamiltonian  $H^{(e)}$  governing the evolution of the vector  $\mathbf{F} = [\psi_2 \psi_3 \psi_4 \psi_6 \psi_7 \psi_8]^T$ :

$$H^{(e)} \mathbf{F} = E \mathbf{F}. \quad (16)$$

The matrix  $H^{(e)}$  is obtained by removing the conduction band rows and columns from  $H$  and updating the parameters  $L$  and  $N_+$  as follows:

$$L(E) = L' + \frac{P^2}{E - E_c - a_c \epsilon}, \quad (17)$$

$$N_+(E) = N'_+ + \frac{P^2}{E - E_c - a_c \epsilon}.$$

Eq. (16) should be solved in each layer of the structure using plane waves. The wavefunctions are then matched at the interfaces by applying the boundary conditions from Burt's envelope function theory<sup>[16]</sup>, which are derived by integrating Eq. (16) across the interfaces. As a result, the vector functions  $\mathbf{F}$  and  $B\mathbf{F}$  must be continuous. The  $6 \times 6$  matrix  $B$  is given by:

$$B = \begin{bmatrix} B_3 & 0 \\ 0 & B_3 \end{bmatrix} \quad (18)$$

where the  $3 \times 3$  block  $B_3$  is defined as:

$$B_3 = \begin{bmatrix} M \partial/\partial z & 0 & iN_- k_x \\ 0 & M \partial/\partial z & iN_- k_y \\ iN_+ k_x & iN_+ k_y & L \partial/\partial z \end{bmatrix}. \quad (19)$$

The solution of  $H^{(e)}$  in each quantum well layer  $n$  is expressed as a superposition of transmitted and reflected plane waves with the same energy  $E$  and in-plane vector  $(k_x, k_y)$ :

$$\mathbf{F} = e^{i(k_x x + k_y y)} \sum_{j=1}^6 \left\{ a_j^{(n)} e^{ik_{zj}^{(n)}(z-z_{z1})} \mathbf{e}_{\pm j}^{(n)} + b_j^{(n)} e^{-ik_{zj}^{(n)}(z-z_{z2})} \mathbf{e}_{-j}^{(n)} \right\}. \quad (20)$$

Here,  $k_{z,j}^{(n)}$  ( $j = 1, \dots, 6$ ) are the  $z$ -components of the complex wave vectors for the bulk states, with positive or zero imaginary parts. The coefficients  $a_j^{(n)}$  and  $b_j^{(n)}$  represent the transmitted and reflected wave amplitudes, respectively, and  $\mathbf{e}_{\pm j}^{(n)}$  are the eigenvectors satisfying:

$$H^{(e)}(\pm k_{z,j}) \mathbf{e}_{\pm j}^{(n)} = E \mathbf{e}_{\pm j}^{(n)} \quad (21)$$

where  $H^{(e)}(\pm k_{z,j})$  matrices are derived from the matrix  $H^{(e)}$  by substituting  $k_z$  with  $\pm k_{z,j}$  where  $k_{z,j}$  satisfy the equation  $|H^{(e)}(k_{z,j}) - EI| = 0$ , with  $I$  representing the identity matrix.

Under the given boundary conditions, the coefficients of two neighboring layers are connected using the transfer matrix. The relationship is expressed as:

$$M^{(n+1)} = \begin{bmatrix} D^{(n+1)} & 0 \\ 0 & I \end{bmatrix} \bar{M}^{(n+1)} \begin{bmatrix} I & 0 \\ 0 & D^{(n+1)} \end{bmatrix} \quad (22)$$

where  $I$  is the  $3 \times 3$  identity matrix, and  $D^{(n)}$  is a  $3 \times 3$  diagonal matrix with elements:

$$D_{ij}^{(n)} = \delta_{ij} e^{ik_{zj}^{(n)}(y_n - y_{n-1})}. \quad (23)$$

Since  $D^{(n)}$  is diagonal, its inverse is obtained by inverting each diagonal element. The matrix  $\bar{M}^{(n+1)}$  is nonsingular and invertible, given by:

$$\bar{M}^{(n+1)} = \begin{bmatrix} \mathbf{e}_+^{(n)} & \mathbf{e}_-^{(n)} \\ \mathbf{f}_+^{(n)} & \mathbf{f}_-^{(n)} \end{bmatrix}^{-1} \begin{bmatrix} \mathbf{e}_+^{(n+1)} & \mathbf{e}_-^{(n+1)} \\ \mathbf{f}_+^{(n+1)} & \mathbf{f}_-^{(n+1)} \end{bmatrix} \quad (24)$$

where  $\mathbf{e}_{\pm}^{(n)} = [\mathbf{e}_{\pm 1}^{(n)} \mathbf{e}_{\pm 2}^{(n)} \mathbf{e}_{\pm 3}^{(n)}]$  and  $\mathbf{f}_{\pm}^{(n)} = [\mathbf{f}_{\pm 1}^{(n)} \mathbf{f}_{\pm 2}^{(n)} \mathbf{f}_{\pm 3}^{(n)}]$ . Additionally:

$$\mathbf{f}_{\pm j}^{(n)} = B \mathbf{e}_{\pm j}^{(n)}. \quad (25)$$

The coefficients of outgoing waves ( $a^{(n)}$ ,  $b^{(n)}$ ) and incoming waves ( $a^{(m)}$ ,  $b^{(m)}$ ) are related through the scattering matrix  $S(m, n)$ :

$$\begin{bmatrix} a^{(n)} \\ b^{(n)} \end{bmatrix} = S(m, n) \begin{bmatrix} a^{(m)} \\ b^{(m)} \end{bmatrix}. \quad (26)$$

Using the transfer matrix equation, a recursive formula for the submatrices of  $S(m, n)$  is derived:

$$S_{11}(1, n+1) = \left[ I - M_{11}^{(n+1)-1} S_{12}(1, n) M_{21}^{(n+1)} \right]^{-1} M_{11}^{(n+1)-1} S_{11}, \quad (27)$$

$$S_{12}(1, n+1) = \left[ I - \right.$$

$$\left. M_{11}^{(n+1)-1} S_{12}(1, n) M_{21}^{(n+1)} \right]^{-1} M_{11}^{(n+1)-1} \left[ S_{12}(1, n) M_{22}^{(n+1)} - M_{12}^{(n+1)} \right],$$

$$S_{21}(1, n+1) = S_{22}(1, n) M_{21}^{(n+1)} S_{11}(1, n+1) + S_{21}(1, n),$$

$$S_{22}(1, n+1) = S_{22}(1, n) M_{21}^{(n+1)} S_{12}(1, n+1) +$$

$$S_{22}(1, n) M_{22}^{(n+1)}.$$

The submatrices of  $M^{(n+1)}$  are obtained as:

$$M_{11}^{(n+1)} = \left[ \bar{M}_{11}^{(n+1)-1} D^{(n)} \right]^{-1}, \quad (28)$$

$$M_{12}^{(n+1)} = D^{(n)-1} \bar{M}_{12}^{(n+1)} D^{(n+1)},$$

$$M_{21}^{(n+1)} = \bar{M}_{21}^{(n+1)},$$

$$M_{22}^{(n+1)} = \bar{M}_{22}^{(n+1)} D^{(n+1)}.$$

By setting  $S(1, 1) = I$ , the recursive relations allow constructing all scattering matrices  $S(1, n)$  for  $n = 2, 3, \dots, N$ . Similarly, setting  $S(m, m) = I$ , all  $S(m, n)$  for  $n > m$  can be constructed.

The coefficients of incoming waves  $a^{(1)}$  and  $b^{(N)}$  are set to zero to determine the energy levels of states confined in the quantum well. Using:

$$M_{11}^{(n+1)} = \left[ \bar{M}_{11}^{(n+1)-1} D^{(n)} \right]^{-1}, \quad (29)$$

$$M_{12}^{(n+1)} = D^{(n)-1} \bar{M}_{12}^{(n+1)} D^{(n+1)},$$

$$M_{21}^{(n+1)} = \bar{M}_{21}^{(n+1)},$$

$$M_{22}^{(n+1)} = \bar{M}_{22}^{(n+1)} D^{(n+1)}.$$

To determine the coefficients for  $n^{\text{th}}$  layer of an  $N$ -layer structure, we have:

$$\begin{bmatrix} a^{(n)} \\ b^{(1)} \end{bmatrix} = S(1, n) \begin{bmatrix} a^{(1)} \\ b^{(n)} \end{bmatrix}, \quad (30)$$

$$\begin{bmatrix} a^{(N)} \\ b^{(n)} \end{bmatrix} = S(n, N) \begin{bmatrix} a^{(n)} \\ b^{(N)} \end{bmatrix}.$$

The coefficients of incoming waves  $a^{(1)}$  and  $b^{(N)}$  are set to zero to determine the energy levels of states confined in the superlattice period. From these, the coefficients  $a^{(n)}$  and  $b^{(n)}$  are determined as:

$$a^{(n)} = \left[ I - S_{12}(1, n) S_{21}(n, N) \right]^{-1} \times \left[ S_{11}(1, n) a^{(1)} + S_{12}(1, n) S_{22}(n, N) b^{(N)} \right], \quad (31)$$

$$b^{(n)} = \left[ I - S_{21}(n, N) S_{12}(1, n) \right]^{-1} \times \left[ S_{21}(n, N) S_{11}(1, n) a^{(1)} + S_{22}(n, N) b^{(N)} \right].$$

To describe the superlattice electronic structure and determine energy levels, periodic boundary conditions must be introduced. For a superlattice, the coefficients of each layer within a period must match the coefficients of the corresponding layer in the next period. For example:

$$\begin{bmatrix} a^{(N)} \\ b^{(1)} \end{bmatrix} = S(1, N) \begin{bmatrix} a^{(1)} \\ b^{(N)} \end{bmatrix}, \quad (32)$$

$$\begin{bmatrix} a^{(1)} \\ b^{(1)} \end{bmatrix} = \begin{bmatrix} a^{(N)} \\ b^{(N)} \end{bmatrix}.$$

As a result, the following equation must be solved to find the energy levels:

$$\left[ S(1, N) - I \right] \begin{bmatrix} a^{(N)} \\ b^{(1)} \end{bmatrix} = 0, \quad (33)$$

or equivalently:

$$|S(1, N) - I| = 0, \quad (1)$$

Once the energy levels of the system are determined, the coefficients  $a^{(n)}$  and  $b^{(n)}$  for each layer can be calculated using the expressions derived above.

## 2 Comparison with experimental results

Using the discussed scattering matrix-based method, we calculated the electronic band-structure of LWIR

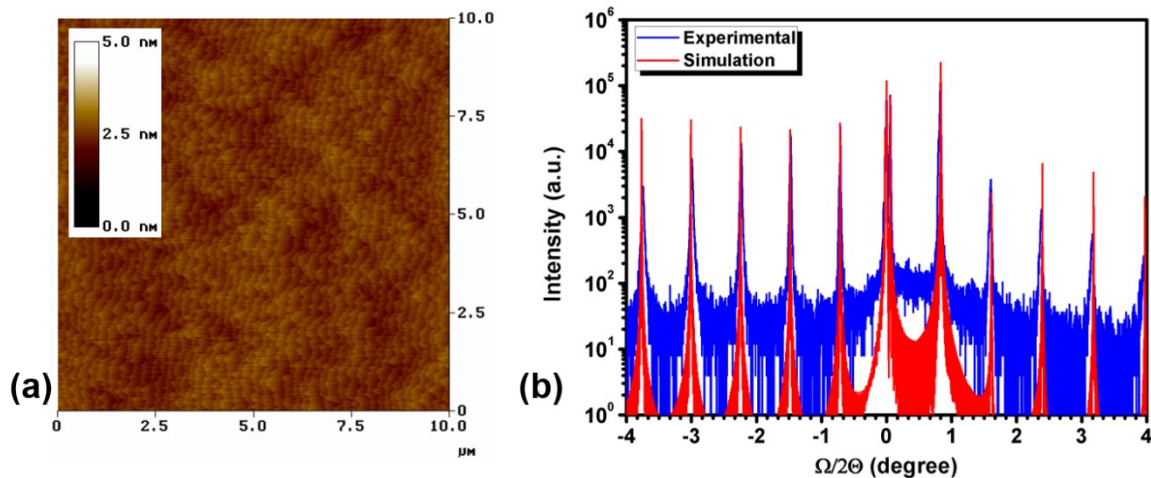


Fig. 1 (a) The atomic force microscopy image of a  $10 \times 10 \mu\text{m}^2$  surface area of one of the LWIR samples used in this study with rms roughness value of  $1.3 \text{ \AA}$ . (b) High-resolution X-ray diffraction (HR-XRD) rocking curve and simulation for the same device.

InAs/GaSb superlattices. The accuracy of the method was validated by comparing calculated cutoff wavelengths to experimental data, demonstrating the precision of this approach.

The samples for this work were grown on *n*-type GaSb substrates using a solid source molecular beam epitaxy (SSMBE) reactor equipped with group III SUMO® cells and group V valved crackers. The quality of the material was assessed after epitaxial growth using atomic force microscopy (AFM) and high-resolution X-ray diffraction (HR-XRD). The samples exhibited good surface morphology, characterized by clear atomic steps and a small surface roughness of less than  $1.5 \text{ \AA}$  over a  $10 \times 10 \mu\text{m}^2$  area, indicating the absence of structural degradation. The satellite peaks in the HR-XRD scan showed the overall periods of the superlattices. The lattice mismatch to the GaSb substrate for all samples was less than 2000 ppm (Figure 1). In Figure 2, we present examples of the photoluminescence (PL) and quantum efficiency (QE) spectra of a photodiode fabricated from one of the LWIR superlattices used in this study at 77 K. The superlattice design consists of 13 and 7 monolayers (MLs) of InAs and GaSb, respectively, with InSb-like interface layers.

The superlattice layer thicknesses for each sample were extracted from HR-XRD results using a method described in Ref. [17] and fed into model to make the electronic band-structure estimation as accurate as possible. The deviations between calculated and measured wavelengths,  $\Delta\lambda = \lambda_{\text{cutoff}} - \lambda_{\text{calc}}$ , are plotted in Figure 3. All samples exhibited deviations within  $0.4 \mu\text{m}$ , with the majority falling below  $0.2 \mu\text{m}$ , highlighting the reliability of this approach.

The thermal effects were also considered, as indicated by red and green lines in Figure 3, which represent the error margin arising from a variation of  $\pm k_B T$  in the bandgap energy at 77 K. Since InAs/GaSb superlattices are often employed as absorbers in infrared detectors operating at 77 K, it is significant that all points lie within these bounds. This alignment underscores that wavelength

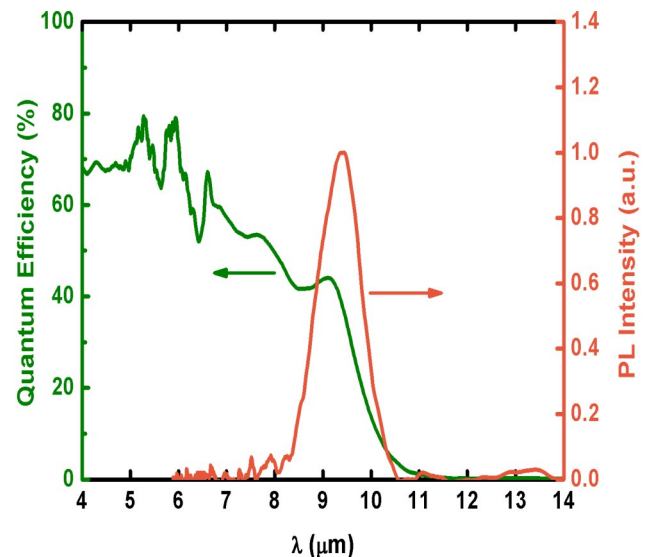


Fig. 2 Quantum efficiency and normalized PL spectra at 77K for one of the LWIR samples used in this study.

deviations are predominantly below typical thermal broadening, further demonstrating the precision of our method.

### 3 Conclusions

We have investigated the electronic band-structure modeling of InAs/GaSb type-II superlattices using a scattering matrix-based approach that incorporates boundary condition matching and interface dynamics. The model's theoretical predictions show strong agreement with experimental results, demonstrating its accuracy in capturing the electronic properties of InAs/GaSb superlattices. These results support the method's effectiveness in providing a detailed understanding of the band structure and its potential utility in the analysis and design of superlattice structures.

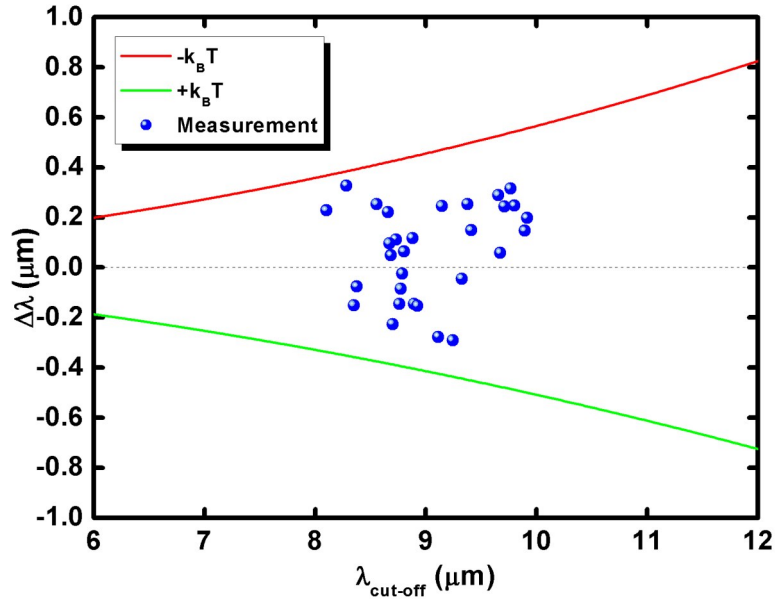


Fig. 3 Deviation of predicted cutoff wavelengths from the measured cutoff wavelengths. The red and green lines indicate the effect of an error of  $k_B T$  in band-gap energy at 77 K.

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