

## Improving measurement accuracy of composite non-point sources emissions based on laser detection

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**Abstract:** In the measurement of source emissions, it is inevitably interfered by the gas emissions from the adjacent fields and turbulence, which affects the accuracy of gas detection. In order to improve the measurement accuracy, the measurement method of composite non-point sources non-uniformity methane emissions based on laser spectrum detection has been studied. Moreover, the interference in external environment is reduced with multiple self-calibration measurements. A detection system for composite non-point source emissions has been established, and the detection method of eliminating gas fluctuation has been proposed. First, the accuracy verification test has been carried out. The standard deviation of source a is 0.17, and that of source b is 0.18. Subsequently, a comparative test has been carried out with the extraction method of the photo acoustic spectrum, and the correlation coefficient reached 0.91. Finally, the actual field measurement has been carried out to monitor the two non-uniform emission sources caused by different fertilization methods to achieve accurate measurement. It has practical engineering value such as agricultural gas emission and environmental gas detection.

**Key words:** laser absorption spectroscopy, accurate measurement, non-uniformity, composite non-point sources

## 基于激光检测提高复合面源排放测量精度研究

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**摘要:**在面源气体排放的测量过程中,不可避免地受到相邻田地气体排放干扰,又受到环境扰动的影响,影响气体检测的准确性。为了提高测量精度,研究了基于激光光谱检测的复合面源甲烷非均匀排放测量方法。通过多次自标定测量,减少了外部环境的干扰。设计了非均匀面源排放物检测系统,并提出了消除气体波动检测方法。首先进行了准确性验证试验,待测源a的标准差为0.17,待测源b的标准差为0.18;随后与光声光谱抽取式进行了对比试验,相关系数达到0.91;最后开展了外场实际的测量应用,对不同施肥方式造成的两个不均匀排放待测源进行监测,实现对多源不均匀排放的准确测量。它具有农业气体排放,环境气体检测等实用工程价值。

**关键词:**激光吸收光谱;准确测量;非均匀;复合面源

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## Introduction

Analysis of global warming potential (GWP) shows that methane is an important greenhouse gas with a global warming potential per molecule 28 times greater than that of carbon dioxide<sup>[1-2]</sup>. The concentration of methane in the atmosphere is greatly affected by human activities<sup>[3-6]</sup>. Therefore, long-term monitoring of methane emission is of great significance for accurate assessment of emission levels. The existing methods for measuring non-point source emission are mainly divided into micro-meteorological method<sup>[7-8]</sup> based optical remote sensing and box method<sup>[9]</sup>. The micro-meteorological detection method based optical remote sensing is a measurement under natural growth state. The tunable diode laser spectroscopy (TDLAS) has the advantages of high sensitivity, real time, fast analysis<sup>[10-12]</sup>, making it an ideal micro-meteorological detection method of gas emission measurement.

In recent years, Thomas K. Flesch has conducted extensive research on the micro-meteorological method based optical remote sensing<sup>[13-14]</sup> and has gradually applied it to the measurement of gas emissions in farmland, pasture, and bio-digester. Yang Wenliang et al.<sup>[15]</sup> used it to study on the monitoring of ammonia emission from farmland. Most of the above studies carried out for measurement analysis. The measurement method of composite non-point sources non-uniformity methane emissions based on laser spectrum detection is studied. A detection system for composite non-point sources emissions is designed. And detection method of eliminating gas fluctuation is proposed. A series of experiments are carried out to verify its accuracy, which has important practical significance for multi-source measurements.

## 1 Measurement principle

According to Beer-Lambert's law:

$$I = I_0 \exp(-S^* \Phi P c L) \quad (1)$$

where  $I_0$  denotes the incident light intensity,  $I$  denotes the transmitted light intensity,  $S^*$  ( $cm^2 atm^{-1}$ ) is the absorption line intensity,  $\Phi$  ( $cm$ ) is the normalized linear function,  $P$  ( $atm$ ) is the total gas pressure,  $c$  (%) is the component concentration of the absorbed gas,  $L$  ( $cm$ ) is the actual optical absorbing path length. and so:

$$c = \frac{1}{S^* \Phi P L} \left( \ln \frac{I_0}{I} \right) = \frac{A}{S^* P L} \quad (2)$$

where  $A$  is the integral absorbance.

The concentration can be inverted by the standard absorption signal and the measured signal obtained by the experimental system, then the measured concentration is expressed as:

$$c = \frac{A}{A_0} \frac{L_0}{L} c_0 \quad (3)$$

where  $c_0$  is the concentration of the standard gas in the

sample cell,  $L_0$  ( $cm$ ) is the optical path length of the standard gas in the sample cell,  $A_0$  is the integral absorbance of the standard gas in the sample cell,  $L$  ( $cm$ ) is the actual optical path length of the experimental system, and  $A$  is the fitted integral absorbance.

When TDLAS is used for long-path open monitoring, the transmitted beam is inevitably affected by turbulence, which causes the intensity fluctuation, the phase fluctuation, the beam expansion, and other phenomena, finally affecting the accuracy of absorption spectrum detection. Then the gas concentration can be expressed as:

$$c(t) = c + \delta(t) \quad (4)$$

where  $\delta(t)$  is the fluctuation.

By using the Eq. (5), the emission rate  $Q$  can be inferred from the concentration at  $M$  and  $(c/Q)_{SIM}$ , and  $c_b$  is the background gas concentration.

$$Q = \frac{c - c_b}{(c/Q)_{SIM}} \quad (5)$$

The  $(c/Q)_{SIM}$  is calculated by summing the reciprocal of the  $w_0$  where the grounding occurs within the source boundary, it can be expressed as Eq. (6).

$$(c/Q)_{SIM} = \frac{1}{n} \sum \left| \frac{2}{w_0} \right| \quad (6)$$

where the variable  $n$  is the total number of calculated particles released from  $M$ , and the sum only covers the touchdown within the source region,  $w_0$  is the vertical velocity at ground contact. Generally, 50000 particles are released by default.

## 2 Detection system for composite non-point sources emissions

The system block diagram is shown in Fig. 1.

The detection system for composite non-point sources is applied to the area to be tested which is composed of the source a and source b to be tested. The system mainly consists of two concentration gas detecting devices (device A and device B) and a three-dimensional sonic anemometer. The device A is integrated with a laser absorption spectrum detecting module, a transceiver telescope, a two-dimensional scanning module, and three corner reflectors. The detection light source uses a DFB laser with the center wavelength at 1 653 nm which is the near-infrared single absorption line of  $CH_4$ . The transceiver telescope and a corner mirror constitute an optical integrated unit of the device A, which is installed on the two-dimensional scanning module. The other two corner mirrors are placed vertically to form a vertical double-angle mirror of device A. Device B is set in the same way.

Device A and device B perform a two-dimensional six path self-calibration scan on source a and source b gases. The laser A generated by the laser absorption spectrum detecting module in the device A is sent to its own transmitting and receiving telescope, which is an op-

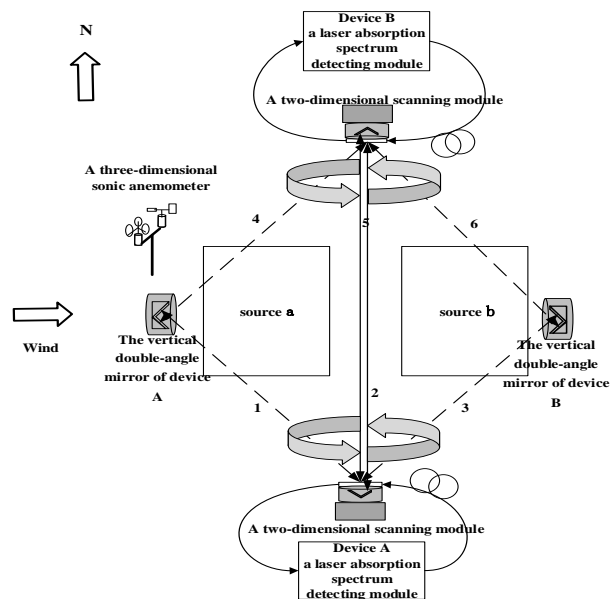


Fig. 1 System layout  
图1 系统布局

tical integrated unit. Three optical paths are scanned by the laser A in one measurement period to form the first optical path, the second optical path, and the third optical path to obtain the concentrations  $c_1(t)$ ,  $c_2(t)$ , and  $c_3(t)$ .

Similarly, the fourth optical path, the fifth optical path, and the sixth optical path are scanned by the laser B in the same measurement cycle to obtain the concentrations  $c_4(t)$ ,  $c_5(t)$ , and  $c_6(t)$ . The second light road and the fifth light road are the common optical path. The background concentration is calculated by  $c_1(t)$  and  $c_4(t)$  based on the unequal precision weights of the two devices. The difference in the gas concentration of the corresponding optical path is obtained by subtracting the background concentration from  $c_2(t)$ ,  $c_3(t)$ ,  $c_5(t)$ , and  $c_6(t)$ .

The WindTrax software is used. Combined with the positional relationship of the detection system, the contribution coefficients of device A and device B are obtained respectively. The gas emission by device A and device B are fused according to different contributions to obtain the  $Q_a$  of the source a and the  $Q_b$  of the source b.

### 3 Detection method and verification of eliminating gas fluctuation

The flow chart of the detection method for eliminating gas fluctuation is shown in Fig. 2. Firstly, the signals from the unabsorbed spectral region in the same period are subjected to two-step fitting. Then, according to the unequal precision, the background signal is obtained and eliminated. Due to external interference, there is still a lot of noise in the signal after removing the background. It needs de-noising, adaptive iterative fitting, and inversion of methane concentration.

Since the second light road and the fifth light road shared the optical path, the two devices can be self-calibrated to correct the concentration. In order to ensure the

accuracy of self-calibration, a sample cell with a known concentration is placed in the detection optical path and used it to calibrate the concentration obtained by the two devices at the same time.

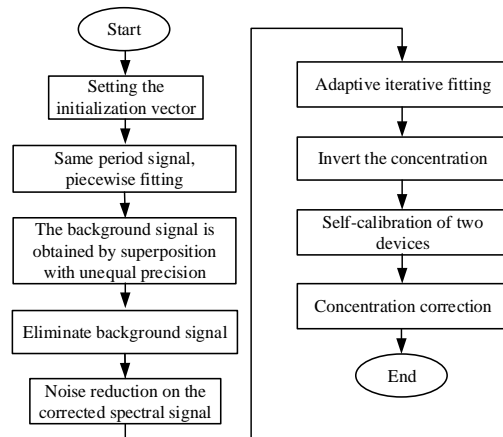


Fig. 2 The flow chart of the detection method for eliminating gas fluctuation  
图2 检测方法流程图

It's shown in Fig. 3 that the proposed method can obtain a more effective background signal in the fitting. Based on the reference spectral data at the same time, the maximum fluctuation of the traditional method is 19.42%, while that of this method is 3.17% (Fig. 4). For the elimination of background noise, the signal-to-noise ratio by the proposed method is significantly better than the traditional fitting method. At the same time, it can also be seen that there is still a lot of noise in the signal after removing the background due to the external disturbance.

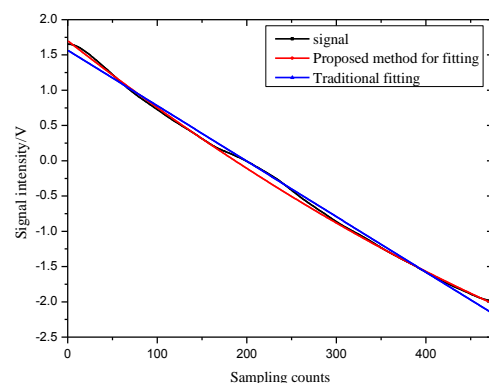


Fig. 3 Fitting for the signal  
图3 信号拟合

The standard absorption curve is reconstructed by adaptive iterative fitting to suppress noise. When performing adaptive iterative fitting, it is achieved by setting the optimal criterion to find the residual difference between the fitting result and the original function. The black curve (Fig. 5) is obtained by de-noising the modified spectral signal, and the fluctuation is obviously re-

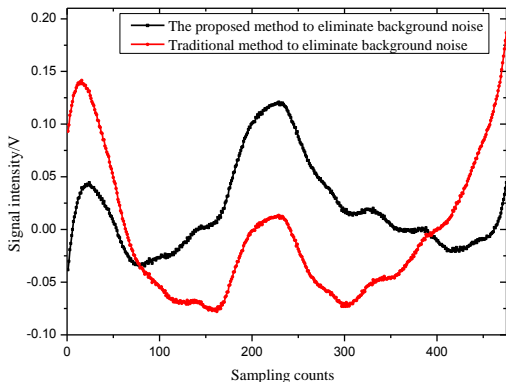


Fig. 4 The background noise elimination  
图4 消除背景噪声

duced. The red curve is obtained by adaptive iterative fitting, and the correlation coefficient reaches 0.977, which verifies its effectiveness.

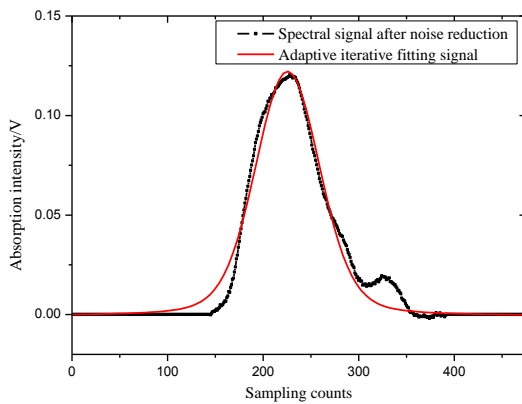


Fig. 5 Adaptive iterative fitting signal  
图5 自适应拟合

## 4 Experimental verification

### 4.1 Verification experiment of the measurement method

The detection system is shown in Fig. 6. The effective length of the first and the fourth optical path is 56 m, the second and fifth optical path are both 58m, the third and sixth optical path are both 56 m. The height of the detection optical path is set to 70 cm.

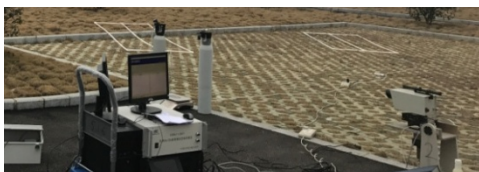


Fig. 6 Experimental site map  
图6 实验现场图

Emissions from different sources are simulated by using two sets of gas simulation volatilization devices.

Experiments are carried out according to different

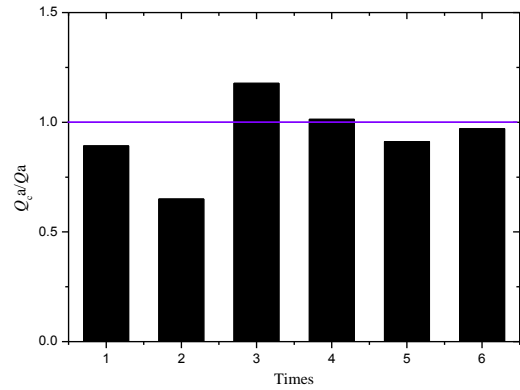


Fig. 7 Accuracy measurement experimental results of source a  
图7 源a的测量实验结果

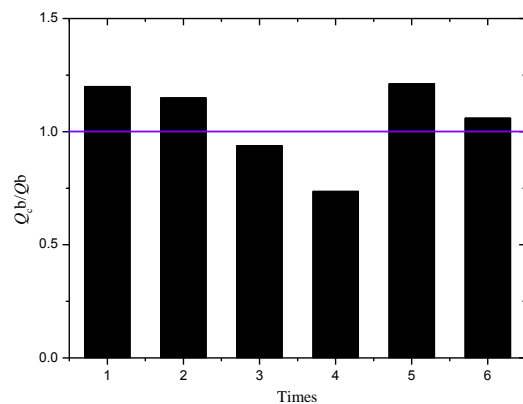


Fig. 8 Accuracy measurement experimental results of source b  
图8 源b的测量实验结果

sources to be tested. Calculate the ratio of the emission to the actual release rate  $Q$  (using Eq. (7).) and compare it with 1. The measurement results of the source a is shown in Fig. 7, and the measurement result of the source b is shown in Fig. 8.

$$Q = \frac{m}{S \times T} \quad , \quad (7)$$

where  $S$  is the area of artificial simulation source,  $T$  is time, and  $m$  is the amount of methane released.

It can be seen from the measurement results that the standard deviation of  $Q_{c a} / Q_a$  for source a is 0.17, and the standard deviation of  $Q_{c b} / Q_b$  for source b is 0.18, which proves its validity.

### 4.2 Comparative experiment

In the comparative experiment, two systems are used to measure the same sources. One of the systems is the designed detection system for composite non-point sources, the other system is the photo acoustic spectroscopy system by extraction mode. System one: Simultaneous measurement of two sources during measurements. System two: First measure the source a, and measure the source b after one-time measurement is completed.

The effective length of the first and fourth optical path is 48 m, the second and fifth optical path are both 50 m, the third and sixth optical path are both 46 m. The height of the detection optical path is set to 73 cm.

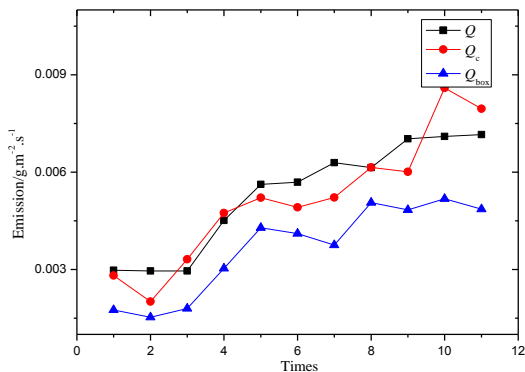


Fig. 9 Experimental results of source a consistency  
图9 源a的一致性实验结果

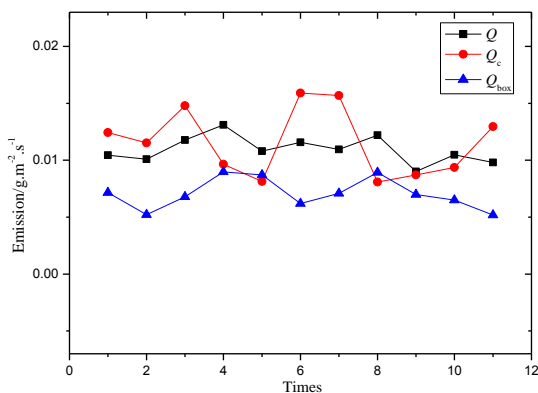


Fig. 10 Experimental results of source b consistency  
图10 源b的一致性实验结果

Correlation analysis is performed by comparing the  $Q$  obtained by different measurement techniques with the actual release rate  $Q$ , as shown in the following figures. It can be seen from the measurement results that the correlation of the two measurement techniques (Fig. 9, 10) is good. However, the box method changes the natural environment, and the spatial representation is poor, resulting in a large measurement error. Compared with the static box method, the proposed method is more flexible, simple, and timely.

### 4.3 Methane monitoring experiment in Fengqiu Ecological Station

The agricultural wheat methane emissions are measured from April 24 to May 4, and the monitoring time lasted for 12 days. The concentration of methane is measured by device A and the device B based on the open-path optical method. Phosphorus fertilizer was applied to source a and biochar was applied to source B respectively, and irrigation was conducted in the same way.

The experimental measurement site is shown in Fig. 11. The effective length of the first and fourth optical path is 98 m, the second and fifth optical path are both 100 m, the third and sixth optical path are both 98 m. The height of the detection optical path is set to 1.4 m.

(1) Continuous observation and analysis of concentration

The methane concentration  $c-c_b$  result is shown in Fig. 12. The measurement was interrupted by Heavy

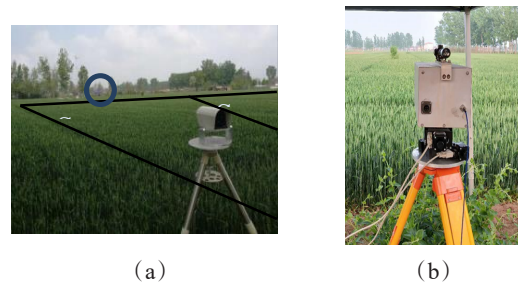


Fig. 11 (a) Experimental site situation, (b)Telescope Experimental site situation  
图11 (a)实验现场图, (b)望远镜

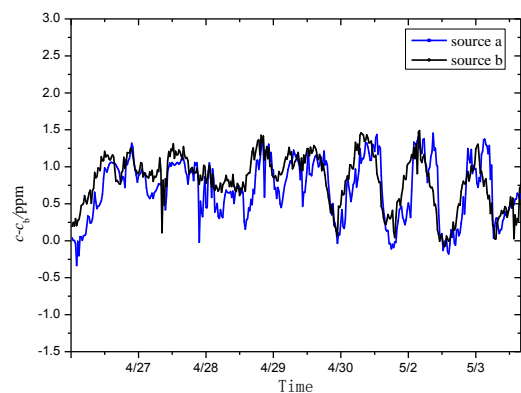


Fig. 12 The methane concentration  $c-c_b$  result  
图12 甲烷  $c-c_b$  结果

rain on the night of the 24 th. Due to the influence of heavy rainfall, the methane emissions from 25 th to 27 th gradually increased and stabilized. After the 29 th, the methane emission of the source a and the source b shows a diurnal variation. The maximum value of the daily average concentration difference for the source a is 1.75 ppm, and the source b is 1.62 ppm.

(2) Analysis of  $Q$  measurement results

It can be seen from Fig. 13 that due to the influence of heavy rainfall, the methane emission of the source a and the source b has a significant downward trend, and

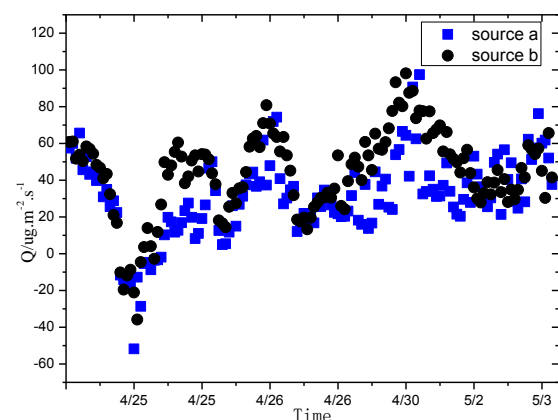


Fig. 13  $Q$  measurement result  
图13 排放结果

then tend to rise. The average of the source a is 31.14 ug/m<sup>2</sup>/s, and the source b is 43.72 ug/m<sup>2</sup>/s. It can be seen from the results that the method can accurately measure the emission of the composite sources.

## 5 Conclusions

In the measurement of source emissions, it is inevitably interfered by the gas emissions from the adjacent fields and turbulence, which affects the accuracy of gas detection. Aiming at the problem, the measurement method of composite non-point sources non-uniformity methane emissions based on laser spectrum detection has been studied. The detection system for composite non-point sources has been designed. And detection method of eliminating gas fluctuation has been proposed. A series of experiments has been carried out.

1 The accuracy verification test has been carried out. The standard deviation of source a is 0.17, and that of source b is 0.18.

2. Compared with the extraction method of the photo acoustic spectrum, the proposed method is more flexible, simple, and timely.

3. The actual field measurement has been carried out to monitor the two non-uniform emission sources caused by different fertilization methods to achieve accurate measurement.

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